

# Improved Performance of a Rectenna Array for Wireless Low Power Transportation

Alexandre Douyère, G Pignolet, J. Riviere, A Verrecchia, G Soulier,  
Jean-Daniel Lan Sun Luk

► **To cite this version:**

Alexandre Douyère, G Pignolet, J. Riviere, A Verrecchia, G Soulier, et al.. Improved Performance of a Rectenna Array for Wireless Low Power Transportation. 68th International Astronautical Congress (IAC), International Astronautical Federation, Sep 2017, Adelaïde, Australia. hal-01696037

**HAL Id: hal-01696037**

**<http://hal.univ-reunion.fr/hal-01696037>**

Submitted on 14 Feb 2018

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

# IMPROVED PERFORMANCE OF A RECTENNA ARRAY FOR WIRELESS LOW POWER TRANSPORTATION

A. Douyère<sup>a\*</sup>, G. Pignolet<sup>a</sup>, J. Rivière<sup>a</sup>, A. Verrecchia<sup>b</sup>, G. Soulier<sup>b</sup> and J.-D. Lan Sun Luk<sup>a</sup>

<sup>a</sup> Laboratory of Electronics, Energetics and Processes (LE2P), University of La Réunion, 15 avenue René Cassin CS 92003, 97744 Saint-Denis Cedex 9 (FRANCE), [alexandre.douyere@univ-reunion.fr](mailto:alexandre.douyere@univ-reunion.fr)

<sup>b</sup> Reunion Island Space Initiative, Saint-Pierre (FRANCE),

\* Corresponding Author

## Abstract

The study presented here focuses on the design of a simple and compact rectenna (rectifying antenna) to enhance the performance at a relatively low power levels. The rectifier is realized with a single schottky diode SMS-7630 in reverse topology and optimised at the fundamental frequency  $f_0 = 2.45$  GHz. Although a single narrow-band design is conductive enough to achieve high efficiency, we know that the amount of the DC output power is limited. To overcome this issue, one solution would be a rectenna array designed for collecting more HF power to produce more DC power. The opportunity in this study would be to increase performances of a ground receiving rectenna, and more precisely for those located on the edges of the array where the RF power density are low. To estimate the DC power, we started with the study of a 2x5 planar array of small metamaterial-inspired antennas. Each antenna incorporates its own rectifier to collect DC power and is assembled in series manner. The size of the overall rectenna array is 110\*90mm<sup>2</sup>. Finally, our most recent studies show an increase of the collected DC voltage with the presence of a reflector at a distance of  $3\lambda/4$  to the back of the rectenna array.

**Keywords:** rectenna array, wireless power transmission, NFRP antenna system [4].

## 1. Introduction

The years pass and we realize that energy is more and more vital for the economic development of the world and is becoming a substantial part of modern societies' everyday life. However, the days of cheap energy seem to be over. Today, the world faces challenges such as climate change, increasing import dependence and higher energy prices. Developing the renewable energy sector is essential if we are to achieve a sustainable and secure energy supply for the future [1].

Solar power collected in space and transmitted to the Earth's surface has been proposed for many years as a potential space option [2,3]. This approach using Wireless Power Transportation (WPT) technology aims to eliminate the cable connections conventionally necessary for transmitting electricity. In a wireless power transmission system, the transmitted energy can be collected by a rectenna system, which consists of two main modules: an antenna and a rectifier. In the receiving side of the energy harvesting process, the RF waves are captured by the antenna which is the key part of the rectenna. The receiving antenna produces an AC signal at its output from the captured microwave radiation. Then, the rectifier converts the received AC current to DC power. The newly successful test results lead the way to applying the technology in numerous terrestrial and space fields. Mitsubishi Heavy Industries, Ltd. (MHI) has recently revived the interest for WPT with a ground-based demonstration testing of a WPT

If the present standard for continuous microwave exposure (20 mW/cm<sup>2</sup>, corresponding to 200 W/m<sup>2</sup>) would be imposed as the upper limit on ground, the average allowed flux on the rectenna would be as small as 100 W/m<sup>2</sup>. Moreover, this flux decreases when moving away from the center, hence the importance of optimizing array performance for low power levels. In this paper an array of ten rectennas has been developed and measured operating at low power levels.

This paper is structured as follows. Section 2 begins with the study of the rectenna design. In this section, all the advantages to the Near-Field Resonant Parasitic (NFRP) antenna design are developed. The optimization of the rectifying circuit at  $f_0=2.45$ GHz, using a single shorted stub and transmission line matching circuit between its input impedance and the antenna impedance, is also presented. Finally, the overall test setup and experimental results on the performance of the array are described and discussed in the subsequent section and also show an increase of the collected DC voltage with the presence of a reflector to the back of the rectenna array.

## 2. Rectenna element design

Rectenna is the third stage of the WPT process. The first studied element of the RF to DC energy conversion system is the receiving antenna.

## 2.1 Antenna design

At low power levels, a high gain antenna is preferable as more RF power can be collected and thus more DC power will be present at load level. The gain of an antenna is however proportional to its equivalent surface. Thus a compromise has to be made between the gain and the surface of the antenna. However, the size of the array must be small to make it practical and inexpensive. In this regard, the antenna element design and its miniaturization play an important role. In this work, a Near Field Resonant Parasitic antenna (NFRP) based on the works of Ning Zhu and Ziolkowski [5] to harvest electromagnetic energy is presented in Fig. 1a. This NFRP antenna may be defined as an electrically small antenna by a weighting factor  $ka = 0.976$  and is designed for ISM band. The antenna is first simulated and then measured using a vector network analyzer (VNA) for this impedance and reflection coefficient  $S_{11}$  (see Fig. 2). The main resonant frequency of the NFRP antenna is located at 2.45 GHz. The -10 dB bandwidth is 20 MHz from 2.35 GHz to 2.55 GHz. Finally, the NFRP antenna allows to reduce the area of the overall rectenna to  $11 \times 50 \text{ mm}^2$  without band pass filter in input.

## 2.2 Rectifier design

The next step is to design the rectifying part of the RF harvesting circuitry. That is, once the antenna receives the input RF signal, it converts a part of the incoming power supply to DC supply voltage. This must be designed in order to achieve the highest total system efficiency. A basic configuration with only one schottky diode for the rectifying circuit is retained as shown in Fig. 3. Commonly called as single-stage rectifier, it consists of a diode connected in series with a capacitor and a load in parallel. The operation of the single stage rectifier is as follows. First, the induced voltage at the output of the matching circuit passes through the schottky diode. The rectified current output is then pumped to the chip capacitor. The energy stored on this capacitor supply the DC power to the load once the rectifier reaches its steady-state mode. The SMS7630 Schottky diode was selected for its zero bias characteristics and its already proven performance at 2.45 GHz. A shunt capacitor of 10 pF, with a quality factor  $Q = 10$  at 2.45 GHz, acts as a filter to smoothen the ripple in the output.

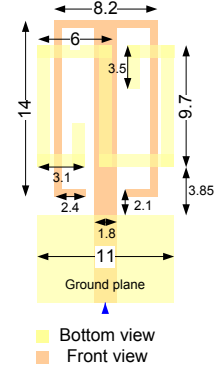


Fig. 1. NFRP Antenna design (mm)

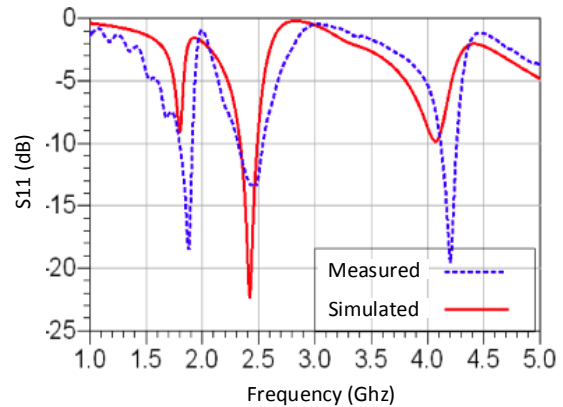


Fig. 2.  $S_{11}$  simulated and measured

In order to optimize the rectenna for maximum power transfer, the antenna impedance must be matched to the impedance of rectifier diode. We propose a matching circuit with a single shorted stub and a transmission line, which is simple and easy to design. This part focuses on the optimization of the rectifier element at low power operation. The diode is matched by the length  $L_1$  of a shorted stub and the length  $T_{L2}$  of a series microstrip line in a narrow bandwidth for the specific RF power. Under a planar method of moments, a tuning optimization method is performed with the software Agilent Advanced Design (ADS), to find the global rectifying circuit. The optimized lengths values are:  $L_1 = 2.9 \text{ mm}$ ,  $T_{L2} = 10.9 \text{ mm}$  and the width of all the lines is fixed to  $50 \Omega$ . The efficiency of the fabricated rectifier at low power levels is depicted in Fig. 4.

The highest conversion efficiency which occurs when the rectifying circuit exhibits a resistive load  $R_{Load} = 3.5 \text{ k}\Omega$  with an optimal efficiency  $\eta_{MAX} \approx 50 \%$  at a collected power  $P_{collected} = -1 \text{ dBm}$ . After the validation of the rectifying circuit and the NFRP antenna separately, the rectenna is realized on the same unit ARLONs AD series substrate with  $\epsilon_r = 3.2$ , a thickness of 0.762 mm and a loss tangent of 0.003.

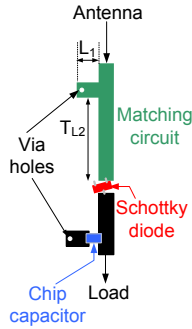


Fig. 3. Layout of the rectifier circuit

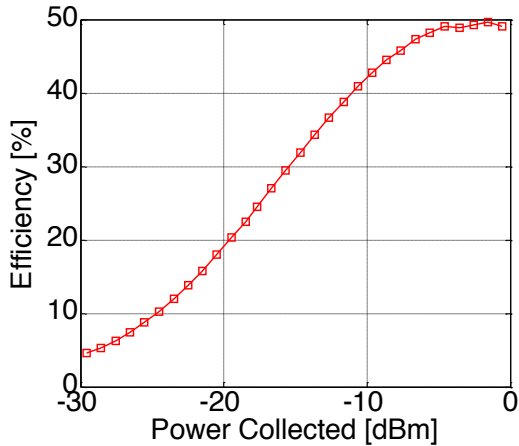


Fig. 4. Measured efficiency for  $R_{Load}=3.5\text{ k}\Omega$

### 3. Array design

Several rectennas can be configured to collect a greater percentage of DC power. The DC power converted independently by each rectenna can then be summed in parallel (current summing), series (voltage summing) or hybrid manner, and is channeled to a power management circuit. Thus, in this study, we consider a compact ten series rectennas array, which is depicted in Fig. 5. A series association allows the increase of the DC output voltage proportional to the number of rectennas but in practice, the results vary slightly due to uncertainty concerning the non-linearity of converter with respect to input power level.

The interelement spacing  $s$  between two rectenna was chosen such that mutual coupling is low (i.e.  $s = 9\text{ mm}$ ,  $|S_{21}| < -10\text{ dB}$ ) [6]. The overall size of the rectennas array is  $110 \times 90\text{ mm}^2$ .

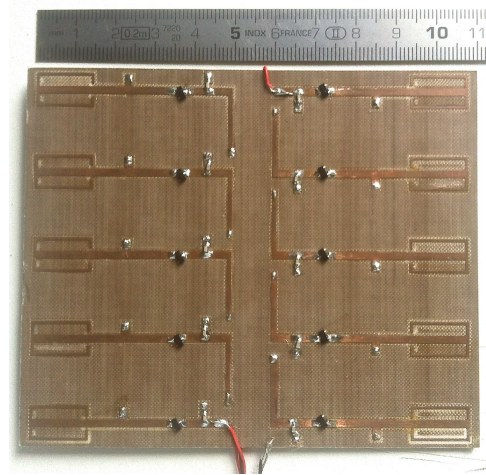


Fig. 5. Rectenna array

### 4. Experimental results

To evaluate the rectenna performance, we use a test system where a transmitting antenna is connected to a HF generator with a fundamental frequency fixed to 2.45 GHz. The performance of the rectenna is verified by measuring the output DC voltage using a digital multimeter with a precision of 0.003% in DC. A linearly polarized bowtie antenna with a gain around +10dB over the frequency of interest is used to provide the RF power. Measurements were performed by placing the proposed rectenna array at a distance of 2 m from transmitting antenna and the source power was set at +25 dBm.

Figure 6 shows the output DC voltage  $V_{out}$  of the rectenna. The maximum output DC voltage is 2.824 V and corresponds to the open-circuit voltage ( $V_{Th}$ ).

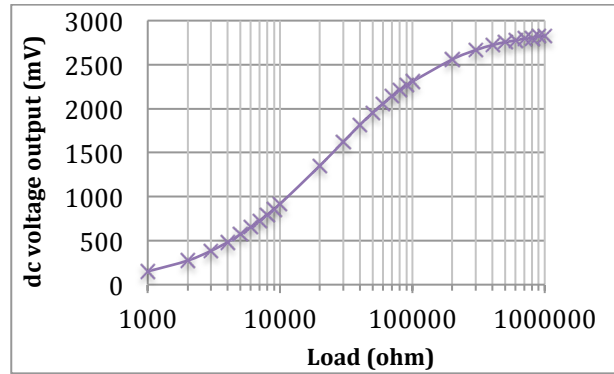


Fig. 6. Output DC voltage

Figure 7 shows the power delivered to the load as a function of  $R_L$ . We notice that the power is small for small or values of  $R_L$  but maximum for some value of  $R_L$  between 0 and  $+\infty$ . The maximum power delivered to the load is  $91\ \mu\text{W}$  with an optimal load  $R_{Lopt}$  of 20 kΩ. According to the maximum power theorem, we know that the maximum power transfer takes place

when the load resistance  $R_L$  equals the Thevenin resistance  $R_{th}$ . The maximum power transfer to the load  $R_L$  can be explain by :

$$P_{MAX} = R_L * i^2 = \left( \frac{V_{Th}}{R_{Th} + R_L} \right)^2 * R_L \quad (1)$$

with  $V_{th} = 2.824V$ ,  $R_{th}=R_L=20 \text{ k}\Omega$ .

With these parameters, the value of  $P_{MAX}$  is about 100  $\mu W$ .

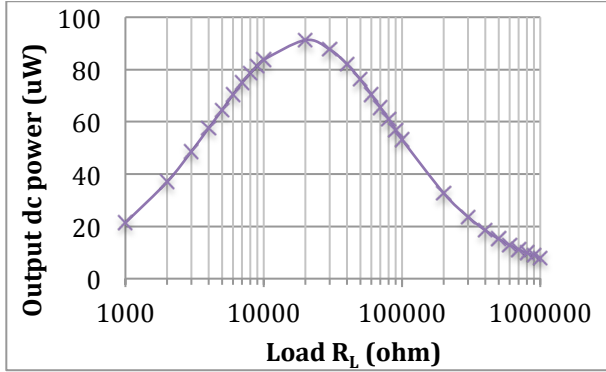


Fig. 7. Output DC power

In practice, for this maximum operating point, if we consider that  $R_{th}=R_L$ , we can conclude that there are about 9  $\mu W$  of internes losses, i.e. about 9%.

A second study was performed using a reflector to the back of the rectenna array. The objective is to increase performance. Indeed, a reflector is relatively inexpensive, offers a higher gain and allows to have a wide bandwidth.

The reflector is moved in a range from 1 cm to 12 cm by step of 1 cm. It appears that maximum of open circuit voltage is reached when the distances are  $\lambda/4$  and  $3\lambda/4$ . We obtain an output DC voltage of 4.5 V at  $\lambda/4$  and about 5V at  $3\lambda/4$  as it is shown on Figure 8.

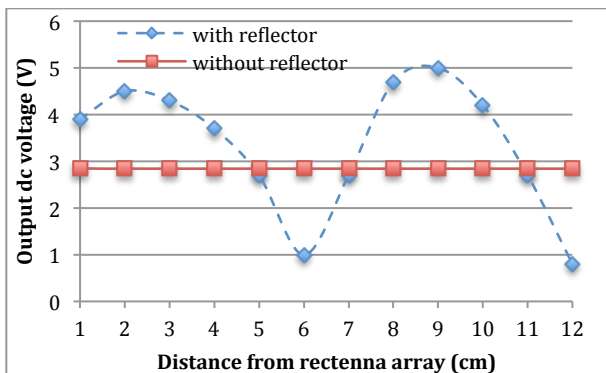


Fig. 8. Impact of the reflector on the output DC voltage

Finally, we can conclude that the optimum distance giving the maximum voltage is  $3\lambda/4$ , which corresponds to a gain of 1.77 on the output dc voltage with a load of  $1M\Omega$ .

## 5. Discussion

This study shows the possibility of achieving a compact and efficient rectenna operating at low power levels. The networking of these rectennas in series topology confirms the increase of the output dc voltage but remains below the theoretical value. Finally, the addition of a reflector to the back of the array at an optimal distance improves performance of the global system.

## 6. Conclusions

This paper reports the design and experimental characterization of a ten rectennas array in the ISM band at 2.45 GHz operating at low power levels. These circuits were achieved in a simple and low-cost manner and experimentally tested. Thus, the results show that using a reflector at 9 cm to the back of the rectenna array, it is possible to increase the collected DC voltage. They present interesting DC output properties and are suitable for another energy harvesting applications.

## Acknowledgements

This work received financial support from Reunion Island Regional Council and European Union - European Regional Development Fund (FEDER).

## References

- [1] Meng-Lin Ku, Wei Li, Yan Chen and K. J. Ray Liu, 'Advances in energy harvesting communications: past, present, and future challenges', *IEEE Communications Surveys & Tutorials*, Vol. 18, N°2, Second Quarter 2016 (doi : 10.1109/COMST.2015.2497324).
- [2] Mankins, John C. "A Fresh Look at Space Solar Power: New Architectures, Concepts and Technologies." 38th International Astronautical Congress, Turin, Italy, 6–10 Oct. 1997. IAF-97 R.2.03.
- [3] Susumu Sasaki and Yoshihiro Naruto, "Guidelines for development of SPS 2000 Educational Model", ISAS, 1999.
- [4] <http://www.mhi.com/news/story/1503121879.html>
- [5] Zhu, N., Ziolkowski, R.W., and Xin, H., 'Electrically small GPS L1 rectennas', *IEEE Antennas Wirel. Propag. Lett.*, 2011, 10, pp. 935–938 (doi: 10.1109/LAWP.2012.2182981).
- [6] Rivière, J., Douyère, A., and Lan Sun Luk, J., D., 'Impact of the coupling effect and the configuration on a compact rectenna array', *IOP Conf. Ser.: Mater. Sci. Eng.*, vol. 67, 012009 (doi:10.1088/1757-899X/67/1/012009).